

Composite / Steel Cost Comparison: Utility

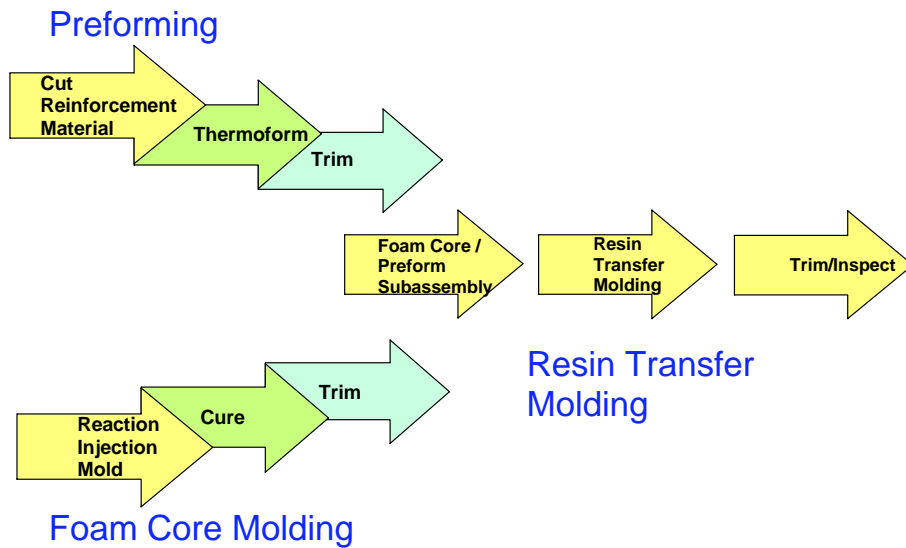
Composites offer the following:

- Advantages
 - Parts Consolidation Opportunities
 - Primary / Secondary Weight Savings
 - Low Investment Costs
 - Increased Design Flexibility
 - Disadvantages
 - Materials and Labor Intensive Process
 - Long Cycle Times
 - Non-traditional Manufacturing Technology
- ➔ **What is the competitive position of composite parts compared to its steel comparator?**

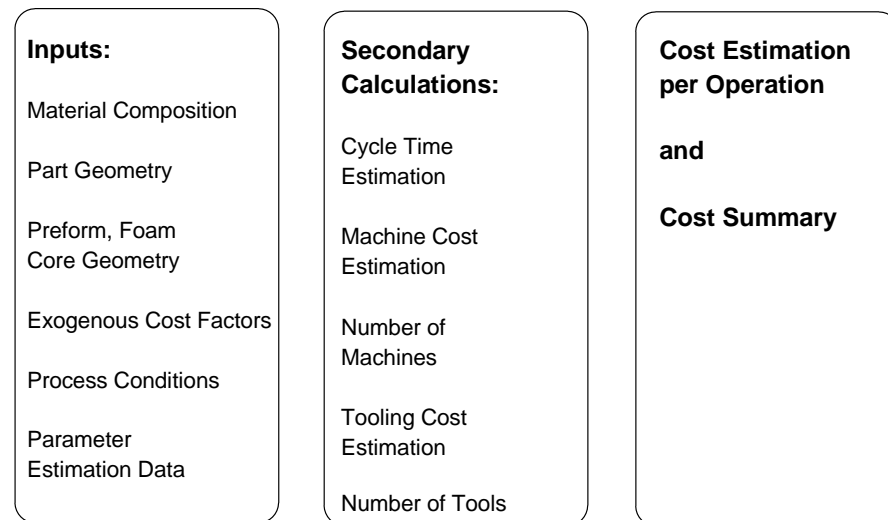
Cost Analysis: Methodology

- Composites Vehicle Design
 - Ford Composite Intensive Vehicle (CIV)
 - Complete Body in White : 8 pieces
 - BIW Weight : approx. 300 kg
- Steel Comparator
 - Honda Odyssey minivan
 - Based on Accord chassis, so comparable size
 - BIW Weight : approx. 400 kg
- Use steel stamping and assembly models to estimate Odyssey's BIW cost
- Use RTM and composites assembly models to estimate CIV's BIW cost
- Identify key process variables, cost drivers, necessary technical improvements

Conceptual Resin Transfer Molding Process Flow



General RTM Cost Model Structure



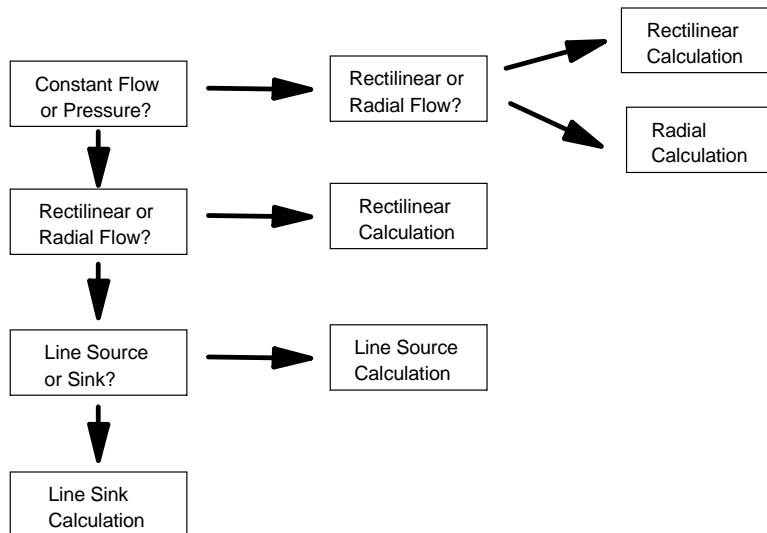
Resin Transfer Molding Cycle Time Estimation

- Cycle Time = Preparation Time + Fill Time + Cure Time
 - Preparation Time:
 - ▶ *Mold Cleaning + Release Agent Coating + Gel Coating + Subassembly Placement + Mold Open/Close + Demold*
 - Fill Time:
 - ▶ *Based on D'Arcy's Law of Flow through Porous Media*
 - ▶ *Six Mold Design Options*
 - ▶ *f(Fiber and Resin Material Properties, Injection Pressure, Mold Geometry)*
 - Cure Time:
 - ▶ *f(Arrhenius constants, Mold Temperature, Percent Conversion)*
 - ▶ *Rate Constants from typical values found in literature*

RTM Fill and Cure Equations

- Fill Time
 - Based on application of D'Arcy's Law: $Q = -(KA/m) dp/dx$, where Q = volumetric flow rate, K =permeability, A =cross-sectional area, m =viscosity and dp/dx = pressure gradient
 - Assumptions:
 - ▶ *Isothermal flow*
 - ▶ *Incompressible, constant viscosity fluid*
 - ▶ *Homogeneous reinforcement*
- Cure Time
 - $dc/dt = (k_1 + k_2 c^m) (1-c)^n$, where c =degree of conversion, k_1 and k_2 are Arrhenius constants, and m, n are empirical constants
 - Assume $m = 0$, $n = 2$,
 - ▶ *Cure Time = $(1/A) \exp(E/RT) \times c/(1-c)$, where A =pre-exponential factor, E =activation energy, R =gas constant, T =mold temperature, c =degree of conversion*

RTM Fill Time Process Flow



RTM Machine and Tooling Cost Equations

- Machine Cost = $C_1 + C_2 \times (\text{Clamping Force Requirement}) + C_3 \times (\text{Platen Area})$
 - C_1, C_2, C_3 : regression constants
 - Clamping Force = $f(\text{maximum injection pressure, mold geometry and mold design})$

- Tooling Cost = $C_1 + C_2 \times (\text{Part Weight}) + C_3 + C_4 \times (\text{Part Surface Area})$
 - C_1, C_2, C_3, C_4 : regression constants, dependent on tool material
 - Tool Material Options
 - *Steel*
 - *Aluminum*
 - *Epoxy*

Effect of Mold Design on Fill Time and Machine Cost

	<u>Fill Time (sec)</u>	<u>Mold Force (N)</u>	<u>Press Cost (\$)</u>
Rectilinear, Constant Flow	12.15	5.4×10^6	\$3,012,346
Rectilinear, Constant Pressure	249.11	4.03×10^5	\$355,782
Radial Source, Constant Pressure	233.45	9.04×10^4	\$176,850
Radial Sink, Constant Pressure	15.54	1.36×10^6	\$903,743

Flow Length = 1.4m (Rectilinear), 0.7m (Radial)
Initial Injection Pressure = 5×10^5 N

RTM Cost Modeling Assumptions

- Materials Prices:
 - Resin (Vinyl Ester) \$2.60 / kg
 - Filler (Calcium Carbonate) \$0.13 / kg
 - Reinforcement:
 - *Glass Fiber CSM* \$2.00 / kg
 - *Carbon Fiber* \$11.00 / kg
 - *Carbon / Glass Blend* \$6.50 / kg
 - Catalyst \$3.24 / kg
 - Foam Core (Polyurethane) \$2.54 / kg

- Foam Core Molding, Thermoforming and RTM Tool Material: Steel

- RTM Flow: Rectilinear, Constant Pressure

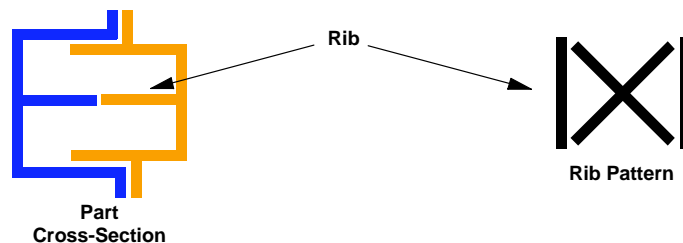
- 32 Steel Inserts

Key Carbon Fiber Design Assumptions for CIV

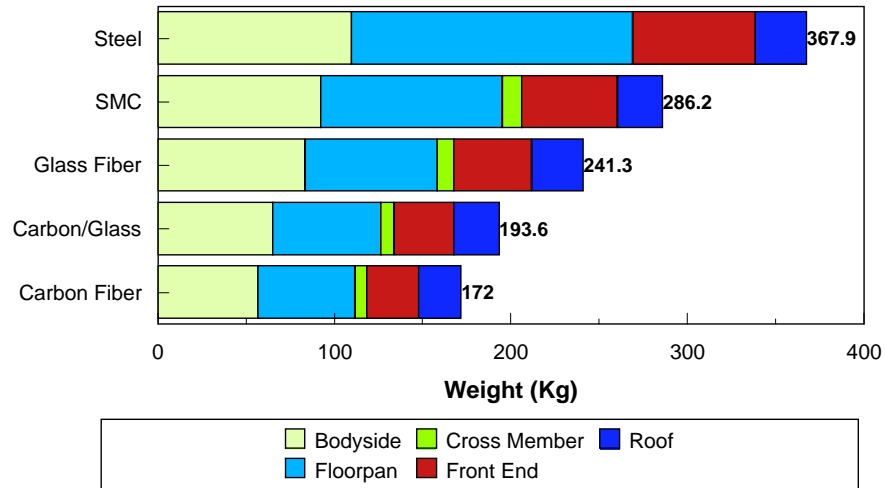
- Use simple beam loading equations to estimate the equivalent thickness of carbon fiber part compared its glass fiber equivalent
- Ratio of moduli determines the thickness of the carbon fiber part
 - Elastic Modulus (Msi):
 - *E glass fiber* : 10.5
 - *Carbon fiber* : 34
 - *Carbon / Glass* : 22.25
 - Part thickness for glass fiber component : 3 mm
- Results
 - Part thickness:
 - *Carbon fiber* : 2.03 mm
 - *Carbon / Glass* : 2.3 mm
 - Relative Weight assuming calculated thicknesses (Glass fiber = 1.0)
 - *Carbon fiber* : 46%
 - *Carbon / Glass* : 65%

Key SMC Design Assumptions for CIV

- SMC part thickness : 4 mm
- Reinforcing rib structure placed every 150 mm
- Reinforcing rib dimensions
 - Length = 150 mm
 - Height and Width are dependent on part geometry
- Foam cores assumed in parts where crush resistance is necessary
 - Front End rails
 - Floorpan
- SMC part is composed of two halves forming a closed section



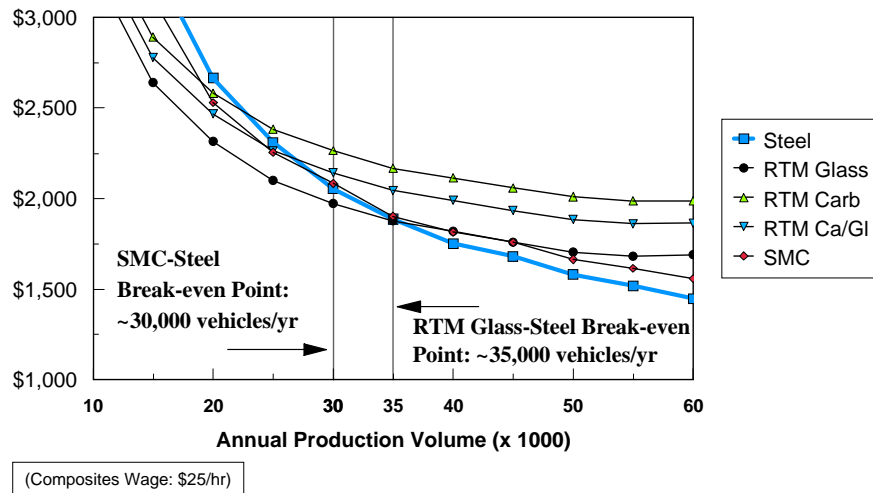
Comparison of Part Weights (including CIV inserts)



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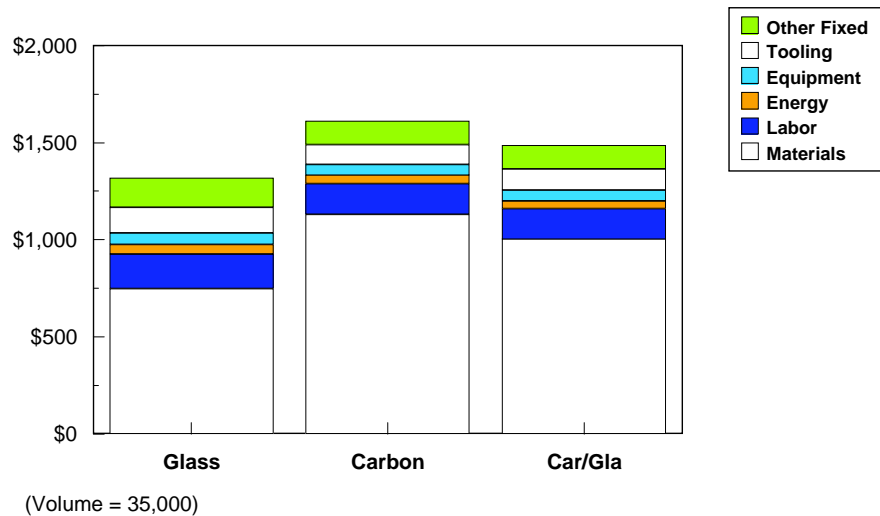
Results: Total Manufacturing and Assembly Cost



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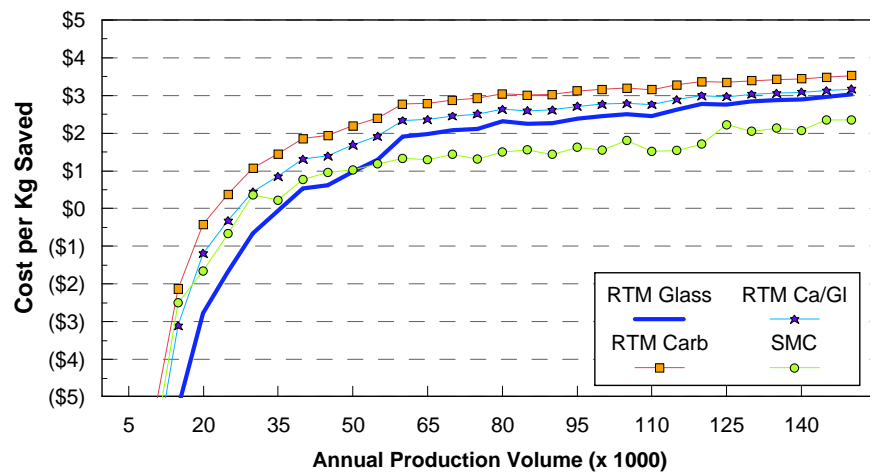
Manufacturing Cost Breakdown: Glass vs Carbon Fiber



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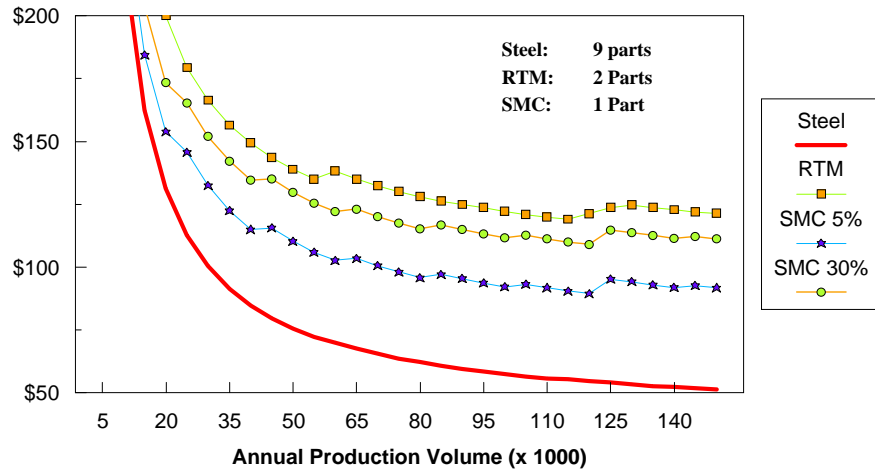
Cost per Kilogram Saved (Relative to Steel Base Case)



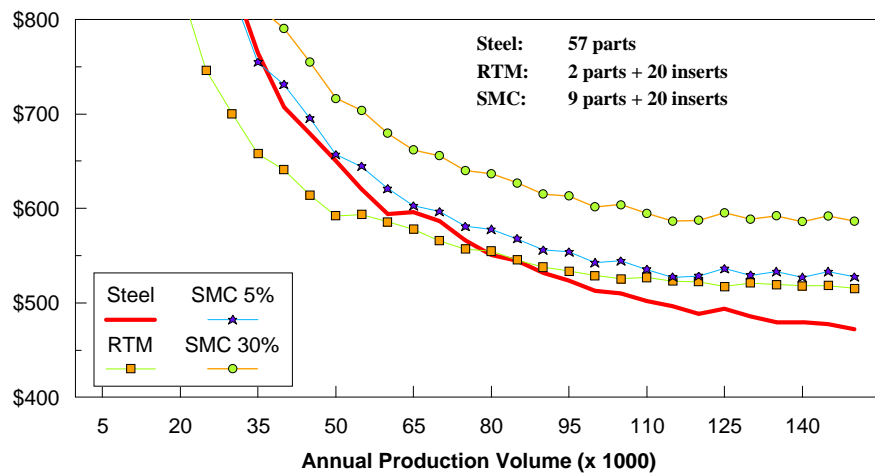
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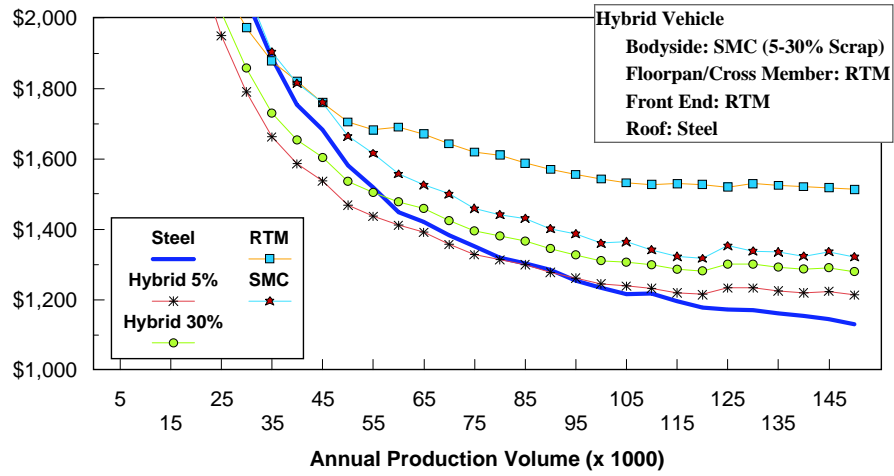
Individual Sub-Systems: Roof



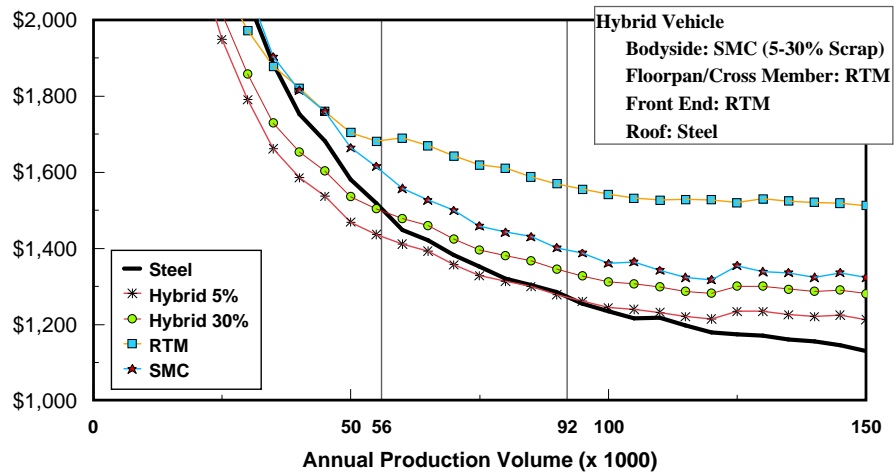
Individual Subsystems: Floorpan/Cross Member



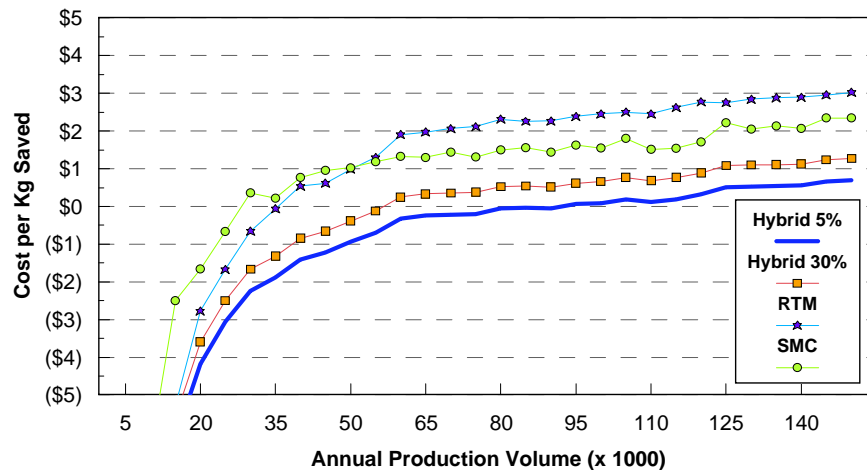
Hybrid Vehicle Scenarios



Hybrid Vehicle Scenarios



Hybrid Vehicles: Cost per Kilogram Saved



Conclusions

- Total cost of composites BIW is competitive with steel at low production volumes (< 40,000 per year)
- Carbon Fiber
 - Use of carbon fiber significantly reduces BIW weight
 - Material price for carbon fiber is too high to justify use in BIW applications
- SMC
 - SMC design requires reinforcing ribs and box sections, which increase weight, tooling costs and assembly costs
 - SMC can be competitive with RTM BIW, given design assumptions
- Subsystems
 - Parts consolidation is a significant advantage for composites
 - ▶ Roof: low parts consolidation, no crossover with steel
 - ▶ Floorpan/Cross Member: high parts consolidation, > 50,000 crossover
 - Designs must minimize material waste
 - ▶ Bodyside: significant consolidation, high material costs => low crossover
- Hybrid vehicles can potentially become competitive with steel at high production volumes